



US006532741B2

(12) **United States Patent**
Watkins

(10) **Patent No.:** **US 6,532,741 B2**
(45) **Date of Patent:** **Mar. 18, 2003**

(54) **GAS GENERATOR FOR PRODUCING ADJUSTABLE FLOW**

H1948 H 3/2001 Rusek et al. 502/344

FOREIGN PATENT DOCUMENTS

(75) Inventor: **William B. Watkins**, Tequesta, FL (US)

WO WO 01/07772 A1 2/2001 F02K/9/74
WO WO 01/07773 A1 2/2001 F02K/9/74

(73) Assignee: **United Technologies Corporation**, Hartford, CT (US)

* cited by examiner

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

Primary Examiner—Ehud Gartenberg
(74) *Attorney, Agent, or Firm*—Brian J. Hamilla

(57) **ABSTRACT**

(21) Appl. No.: **09/896,608**

(22) Filed: **Jun. 29, 2001**

(65) **Prior Publication Data**

US 2003/0000200 A1 Jan. 2, 2003

(51) **Int. Cl.**⁷ **F02C 7/00**

(52) **U.S. Cl.** **60/723; 60/259; 60/39,462**

(58) **Field of Search** 60/218, 259, 39,462, 60/723

A gas generator, comprising a catalyst section and a mixer section. The catalyst section has openings through which a material enters and reacts with a catalyst to decompose and to produce heat. The mixer section, located downstream of the catalyst section, introduces an additional amount of the material. The heat produced in the catalyst section is sufficient to decompose the additional amount of material introduced into the mixer section without exposure to said catalyst. The catalyst bed assembly could be part of a turbopump assembly. A nozzle downstream of the mixer section directs the exhaust towards a turbine. The turbine drives a pump. The amount of material added to the mixer is selected to produce a desired amount mass flow through the nozzle. Adding material to the mixer causes the turbopump to supply more fuel or oxidizer to a rocket engine. Thus, the rocket engine is throttleable.

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,488,962 A * 1/1970 McCormick 502/302
4,731,989 A * 3/1988 Furuya et al. 431/7
5,573,736 A 11/1996 Jubin, Jr. 422/191
6,000,212 A * 12/1999 Kolaczowski et al. 431/7

5 Claims, 9 Drawing Sheets

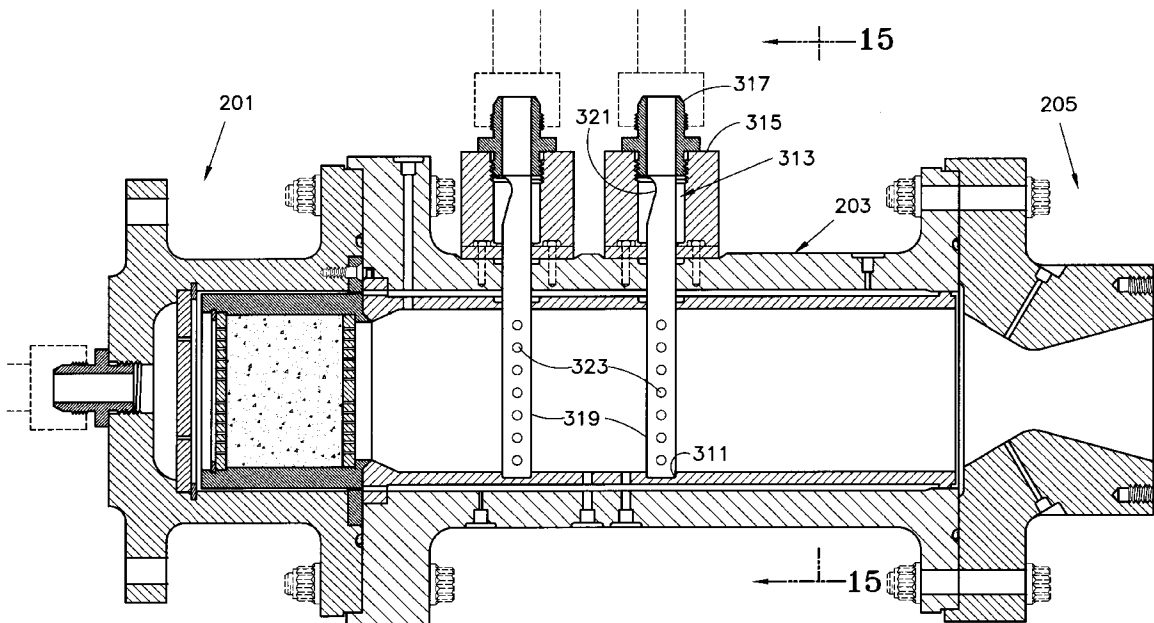


FIG. 1

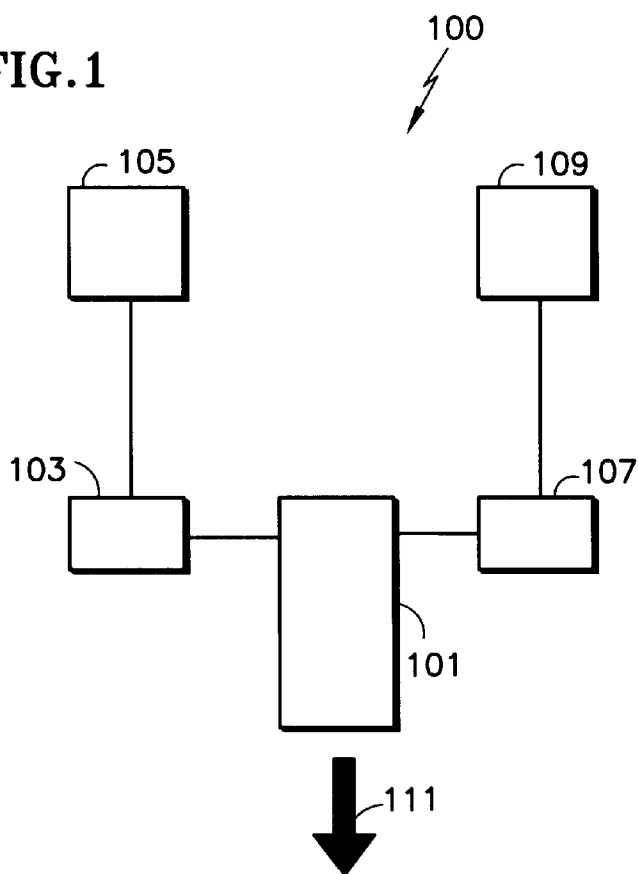


FIG. 2

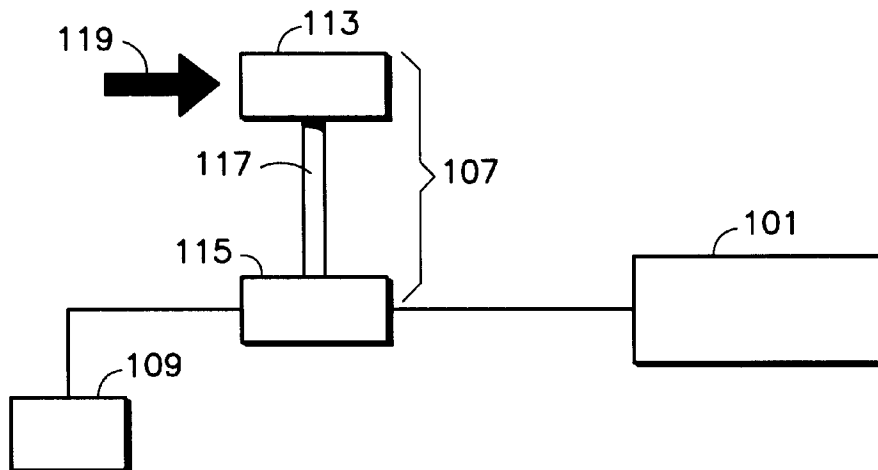


FIG. 3

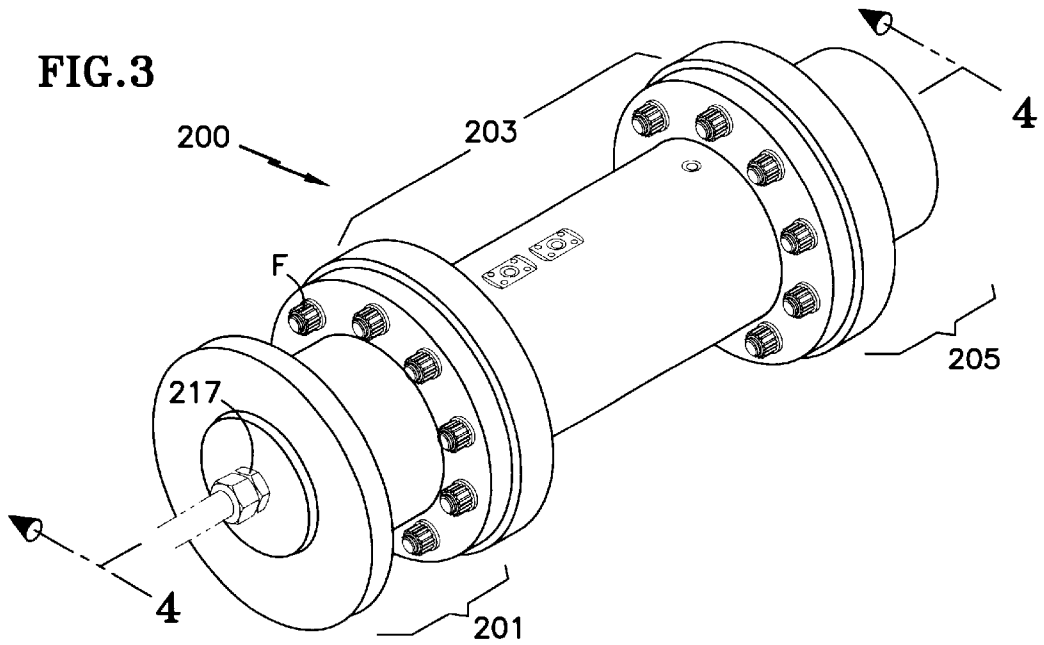
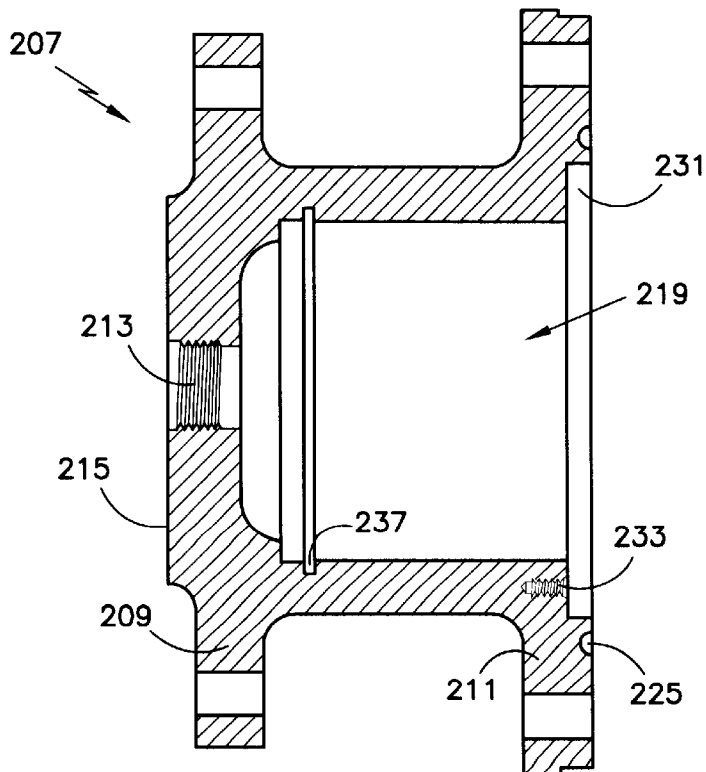


FIG. 5



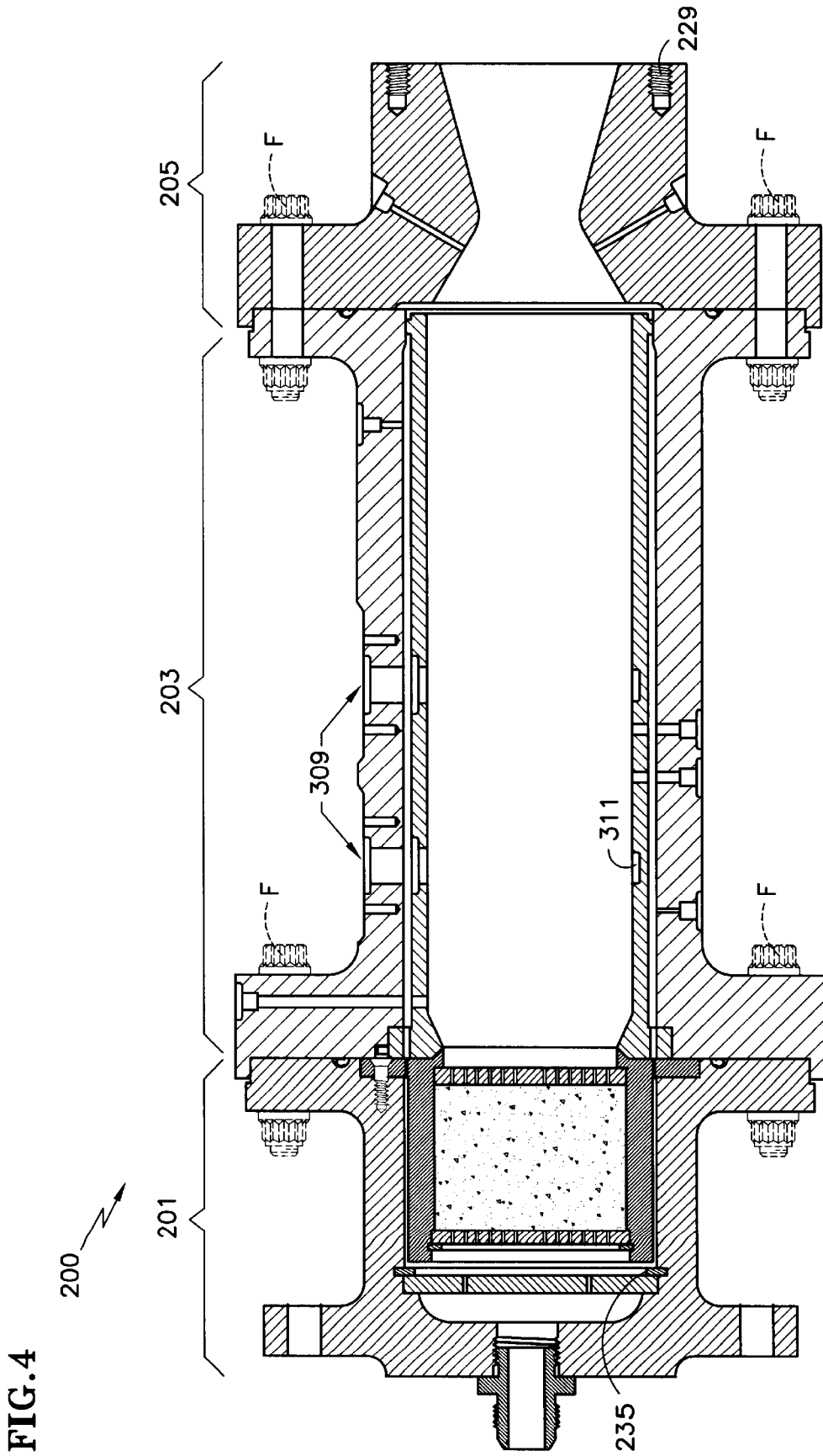


FIG. 6

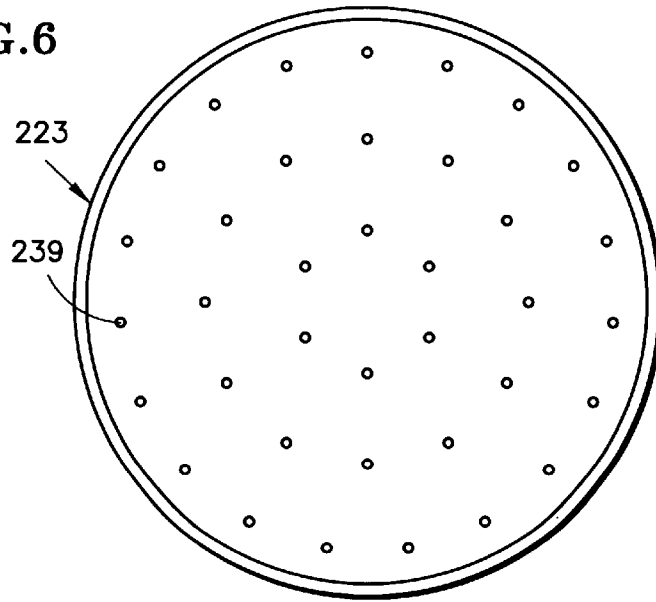


FIG. 9

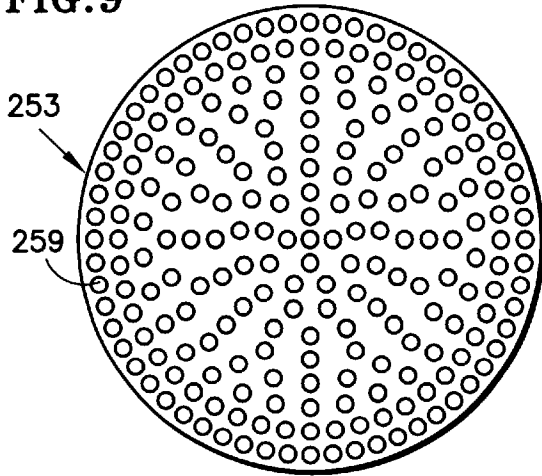


FIG. 10

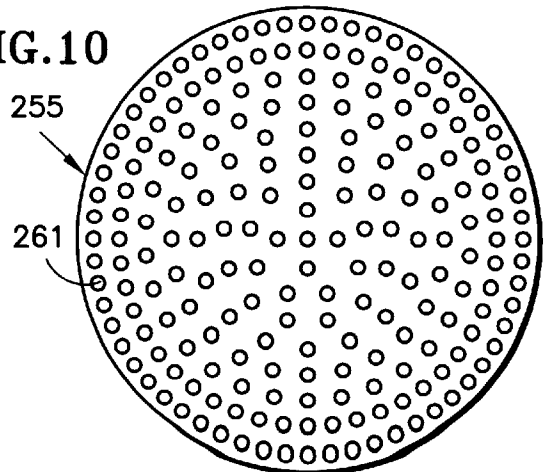


FIG. 7

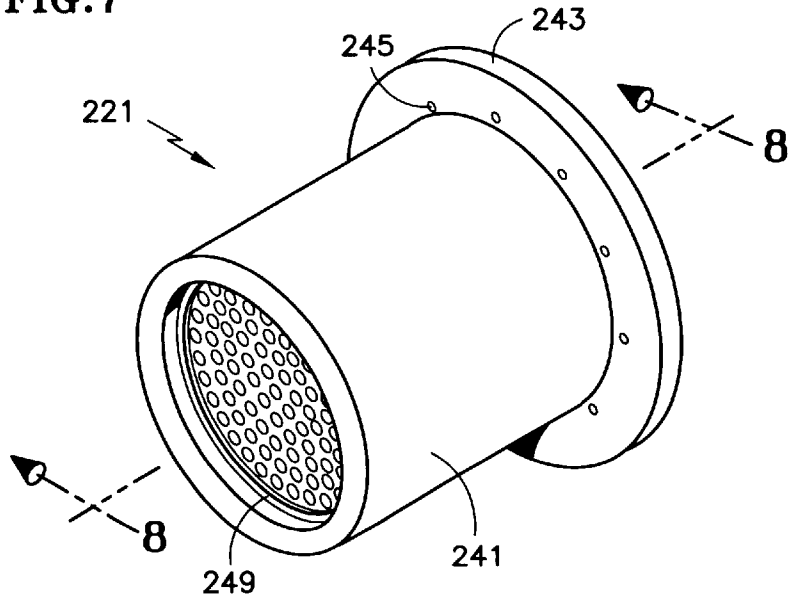
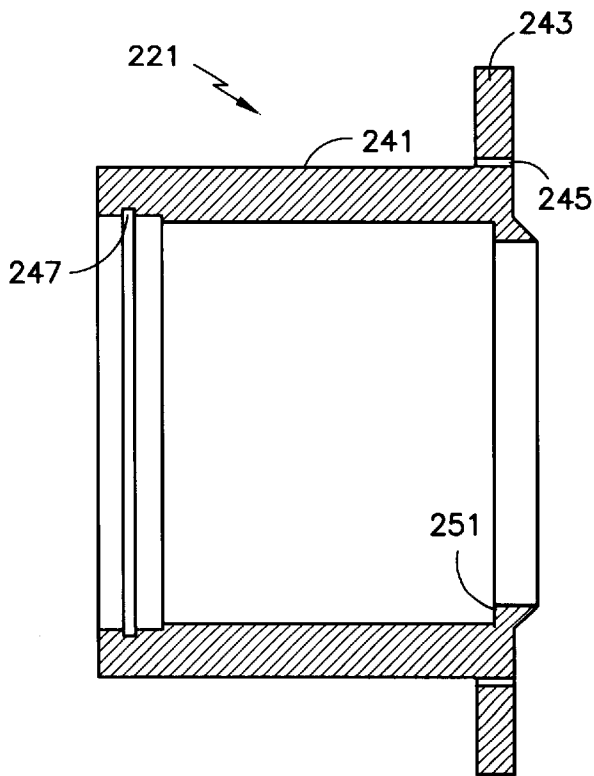


FIG. 8



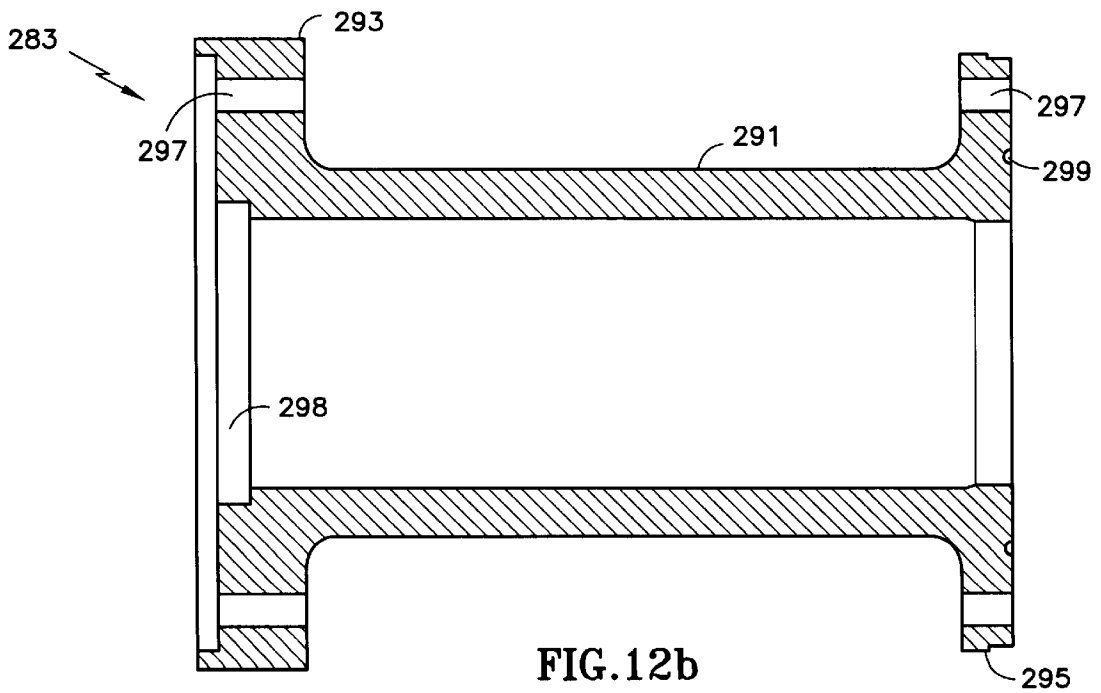
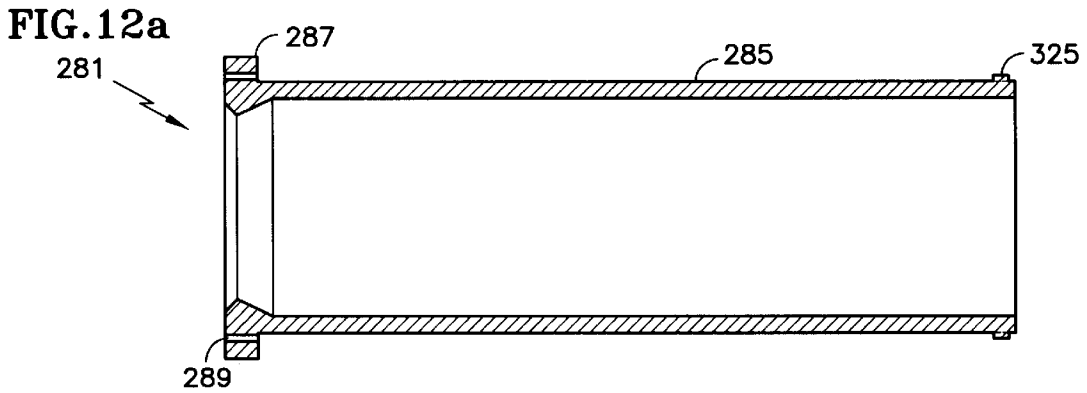
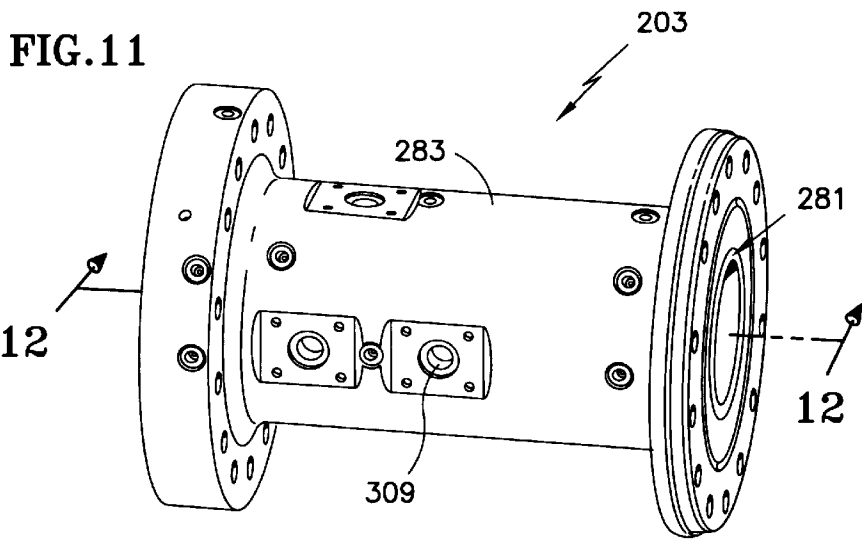
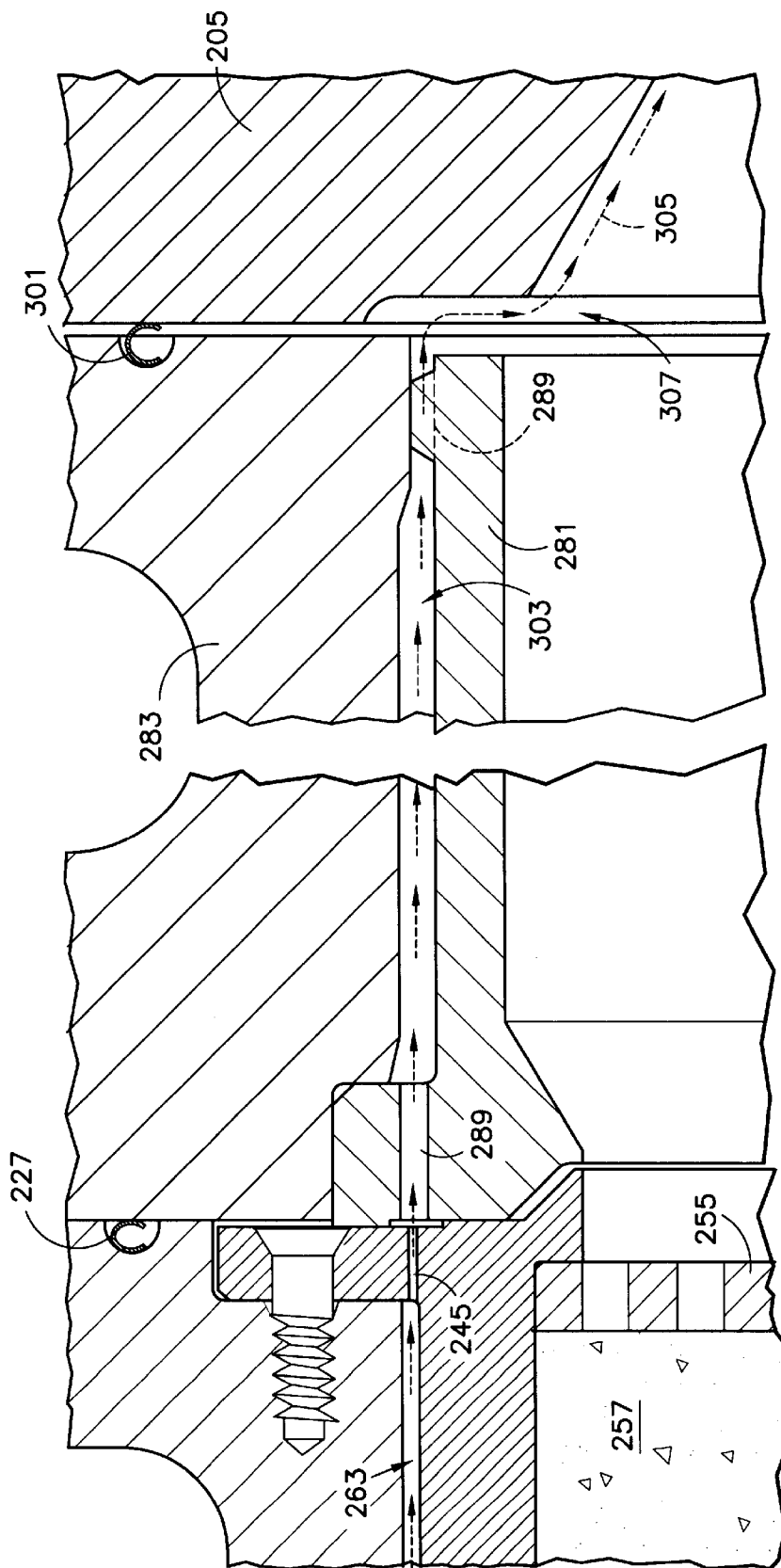


FIG. 13



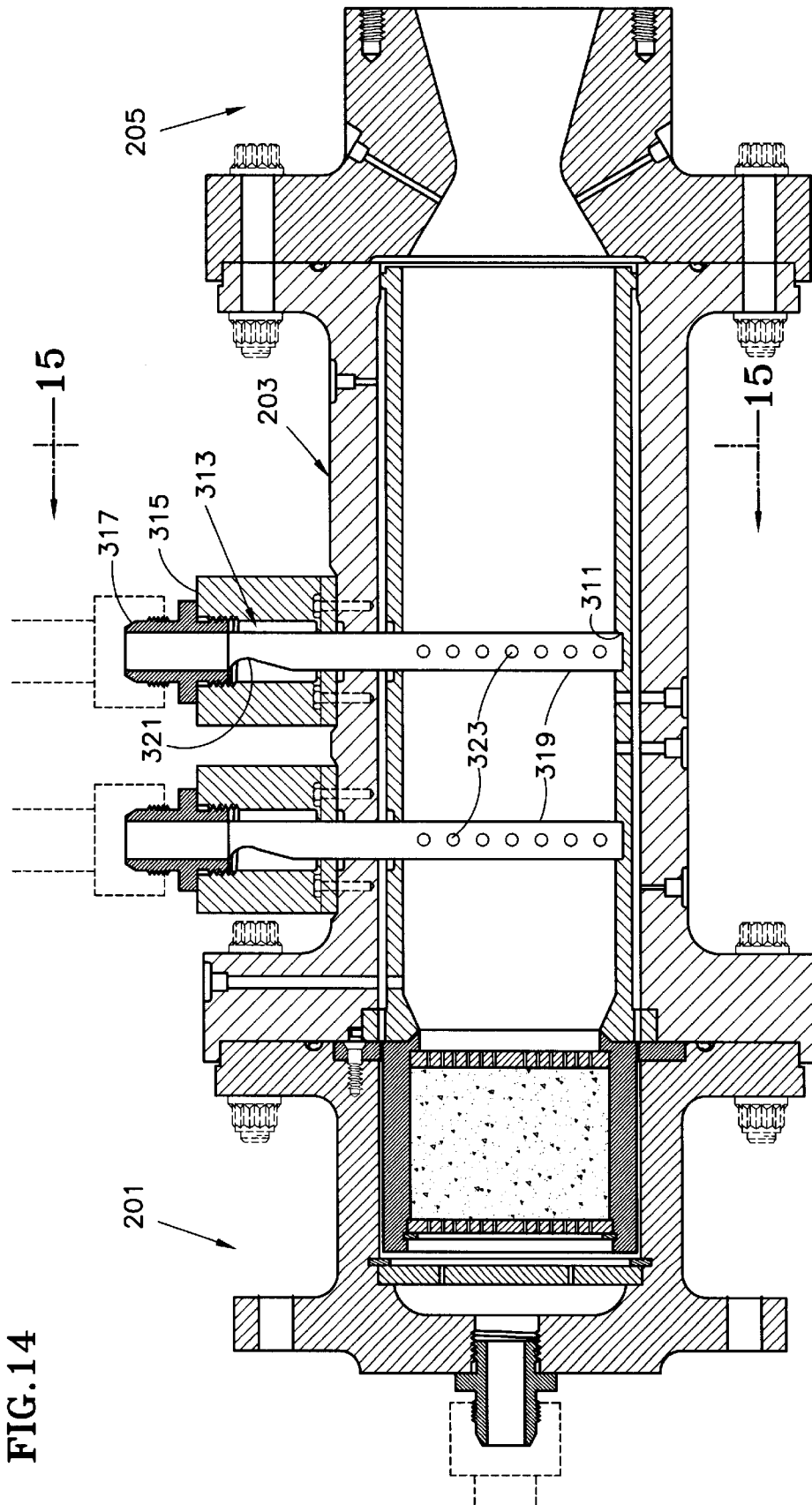
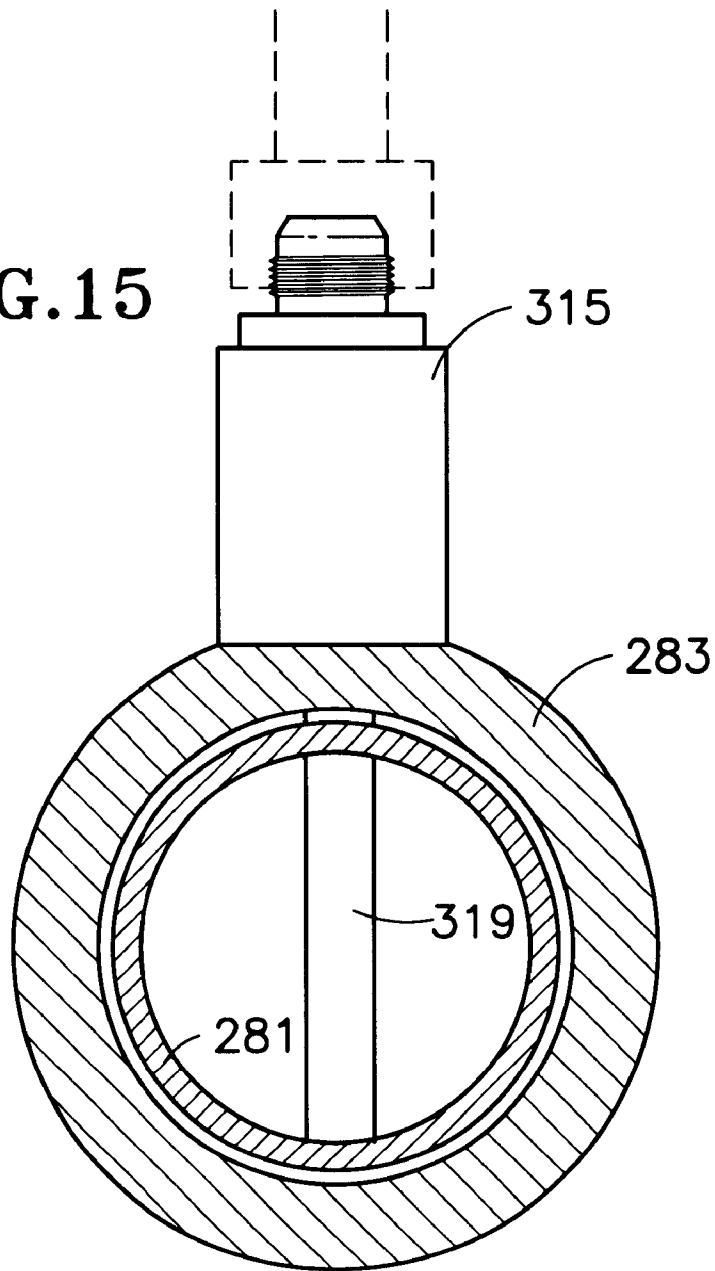


FIG. 14

FIG. 15



GAS GENERATOR FOR PRODUCING ADJUSTABLE FLOW

RELATED APPLICATIONS

This application is related to United States Patent Application number 09/896,355 filed on even date, herein incorporated by reference.

TECHNICAL FIELD

This invention relates to rocket engines. More particularly, this invention relates to a gas generator that can produce an adjustable flow so as to throttle the rocket engine.

BACKGROUND OF THE INVENTION

FIG. 1 is a schematic of a rocket propulsion system **100**. The system **100** includes a rocket engine **101**. A fuel pump **103** supplies fuel to the rocket engine **101** from a fuel supply **105**. Likewise, an oxidizer pump **107** supplies oxidizer to the rocket engine from an oxidizer supply **109**. The rocket engine **101** combines the fuel and oxidizer, and ignites the mixture in a combustion chamber (not shown). The exhaust **111** exits a nozzle (not shown) to produce thrust.

To provide the amount of fuel and oxidizer required by the rocket engine **101**, pumps **103**, **107** are preferably turbopumps. FIG. 2 is a schematic of a turbopump assembly **107**. Generally speaking, the turbopump assembly **107** includes a turbine **113** connected to an impeller **115** by a shaft **117**. The turbine **113** converts the kinetic energy from an exhaust stream **119** into shaft horsepower to drive the impeller **115**. The impeller **115** transports the oxidizer from the supply **109** to the rocket engine **101**. Turbopump **103** for the fuel operates in a similar manner, and is not described in further detail.

In conventional operations, the turbopumps **103**, **107** provide a constant supply of oxidizer and fuel to the rocket engine **101**. This uniform supply of oxidizer and fuel by the turbopumps **103**, **107** produces a constant thrust in the rocket engine **101**.

DISCLOSURE OF THE INVENTION

It is an object of the present invention to provide a rocket engine having adjustable thrust.

It is a further object of the present invention to provide a turbopump assembly that can adjust the thrust of a rocket engine.

It is a further object of the present invention to provide a turbopump assembly having a gas generator having a mixer section that can adjust output flow.

It is a further object of the present invention to provide a gas generator with a catalyst bed section that decomposes a material upon exposure to a catalyst and a mixer section that decomposes the material without exposure to a catalyst.

It is a further object of the present invention to provide a gas generator with a catalyst bed section that decomposes a material upon exposure to a catalyst and a mixer section that thermally decomposes a material without exposure to a catalyst.

It is a further object of the present invention to provide a gas generator having a catalyst bed assembly and which bypasses a portion of a material around the catalyst bed section for cooling.

These and other objects of the present invention are achieved in one aspect by a gas generator. The gas generator

comprises: a catalyst section including openings through which a material enters and reacts with a catalyst to decompose and to produce heat; and a mixer section downstream of the catalyst section, the mixer section introducing an additional amount of the material. The heat produced in the catalyst section is sufficient to decompose the additional amount of the material without exposure to the catalyst.

These and other objects of the present invention are achieved in another aspect by a turbopump assembly. The turbopump assembly comprises: a catalyst bed for decomposing a material to produce a discharge; a mixer section downstream of the catalyst bed for introducing an additional amount of the material to the discharge to produce an exhaust stream having a mass flow; a nozzle downstream of the mixer section; a turbine downstream of the nozzle; and a pump driven by the turbine. The additional amount of the material is selected to produce a desired amount of mass flow.

These and other objects of the present invention are achieved in another aspect by a method of throttling a rocket engine. The method comprises the steps of: providing a catalyst bed; introducing an amount of a material into the catalyst bed so that the catalyst bed decomposes the material to produce a discharge; and selectively adding an additional amount of the material into the discharge to produce an exhaust stream having a mass flow. The additional amount of material increases the mass flow of the exhaust stream.

BRIEF DESCRIPTION OF THE DRAWINGS

Other uses and advantages of the present invention will become apparent to those skilled in the art upon reference to the specification and the drawings, in which:

FIG. 1 is a schematic of the components of a rocket propulsion system;

FIG. 2 is a schematic of a turbopump assembly;

FIG. 3 is a perspective view of a partially assembled gas generator of the present invention;

FIG. 4 is a cross-sectional view of the gas generator of FIG. 3 taken along line IV—IV;

FIG. 5 is a cross-sectional view of the outer housing of the catalyst bed section;

FIGS. 6, 9 and 10 are front views of pressure baffles used in the catalyst bed assembly of FIG. 3;

FIG. 7 is a perspective view of the catalyst can of the catalyst bed section;

FIG. 8 is a cross-sectional view of the catalyst can of FIG. 7 taken along line VIII—VIII;

FIG. 11 is a perspective view of the mixer section;

FIGS. 12a and 12b are cross-sectional views of the components of the mixer section of FIG. 11 taken along line XII—XII;

FIG. 13 is a detailed cross-sectional view of the gas generator of FIG. 4;

FIG. 14 is a cross-sectional view of a fully assembled gas generator; and

FIG. 15 is a cross-sectional view of the gas generator of FIG. 14 taken along line XV—XV.

BEST MODE FOR CARRYING OUT THE INVENTION

FIG. 3 is a perspective view of a partially assembled gas generator **200** of the present invention. The gas generator **200** includes several sections. Starting from the upstream

end, the gas generator **200** has a catalyst bed section **201**, a mixer section **203** and a nozzle section **205**. Fasteners **F** can secure the various sections **201**, **203**, **205** of the gas generator **200** together in a conventional manner.

FIG. 4 displays a cross-sectional view of the gas generator **200**. Generally speaking, the catalyst bed section **201** decomposes a highly concentrated (e.g. 98 wt-%) hydrogen peroxide using a catalyst material. The mixer section **203** receives the discharge from the catalyst bed section **201**, namely water vapor, oxygen and heat. The mixer section **203** introduces a selected additional amount of hydrogen peroxide to the discharge. This additional hydrogen peroxide decomposes without exposure to the catalyst material, i.e. due to the temperature of the discharge. The nozzle **205** receives the discharge from the mixer **203** to produce an exhaust stream. The additional hydrogen peroxide injected into the mixer **203** augments the discharge from the catalyst bed section **201**. The amount of additional hydrogen peroxide used is selected to produce a desired mass flow of the exhaust stream. Each section of the gas generator **200** will now be described in greater detail.

As seen in FIG. 4, the nozzle section **205** resides at the downstream, or outlet, end of the mixer **203**. The nozzle **205** receives the output from the mixer **203**, and accelerates the output from the mixer **203** to form the exhaust stream **119**. As described earlier, the exhaust stream **119** leaving nozzle **205** can drive the turbine **113** in the turbopump **107**. Although shown as a convergent-divergent nozzle, the present invention could use any suitable nozzle arrangement.

The nozzle **205** can have threaded openings **229** for securing to the turbopump **107**. Also, the nozzle **205** could be made from any suitable material, such as a high temperature, non-catalytic aerospace alloy.

The catalyst bed section **201** includes a catalyst can **221** within an outer housing **207**. As seen in FIG. 5, the outer housing **207** can be a cylindrical pipe having flanges **209**, **211** to secure the catalyst bed section **201** to other components. However, other arrangements are possible. Outer housing **207** could be made from any suitable material, such as a high temperature, non-catalytic aerospace alloy.

The outer housing **207** secures to mixer **203** using fasteners **F**. As seen in FIG. 5, flange **211** includes an annular groove **225** within which a C-shaped (in cross-section) annular metal seal **227** resides. The seal **227** keeps the decomposed hydrogen peroxide from escaping from the joint between the catalyst bed section **201** and the mixer **203**. Although described as a metallic C-shaped annular seal, any suitable seal or sealing arrangement could be used.

The outer housing **207** includes a threaded opening **213** in a front face **215**. The opening receives a correspondingly threaded coupling **217** to create an inlet. The coupling **217** secures to a pipe (shown in phantom in FIG. 3) supplying liquid hydrogen peroxide to the gas generator **200**.

The outer housing **207** includes an open interior **219**. The open interior **219** has a suitable size to receive a catalyst can **221**. As seen in FIG. 5, the outer housing **207** has an annular shoulder **231** in which a portion of the catalyst can **221** rests. The outer housing **207** also has at least one threaded opening **233** for securing the catalyst can **221** on the shoulder **231** with a suitable fastener (not shown).

A first pressure baffle **223** resides within the open interior **219** of the outer housing **207**. The pressure baffle **223** is preferably made from a high temperature, non-catalytic aerospace alloy. As seen in FIG. 6, the baffle **223** has an array of openings **239** therethrough. Preferably, the baffle

223 has an outer diameter of approximately 3.96" and the openings **239** have a diameter of approximately 0.063". However, other sizes, numbers and arrangements of the apertures could be used to achieve a suitable result. A ring **235** placed in an annular groove **237** on the inner surface of the outer housing **207** retains the pressure baffle **223** within the outer housing **207**.

The baffle **223** reduces the pressure of the liquid hydrogen peroxide in the direction of flow. In other words, the pressure of the hydrogen peroxide downstream of the baffle **223** is less than the pressure of the hydrogen peroxide upstream of the baffle.

Although the decomposition of the hydrogen peroxide in the catalyst can **221** produces a temperature of approximately 2192° R, neither the outer housing **207**, the mixer **203** nor the nozzle **205** require any external cooling lines. Rather, the present invention uses bypass hydrogen peroxide (i.e. hydrogen peroxide that does not enter the catalyst can **221**) to travel within the gas generator **200** and to cool the catalyst bed section **201**, the mixer **203** and the nozzle **205**. In the catalyst bed section, a gap **263** exists between the catalyst can **221** and the outer housing **207**. The gap **263** allows some hydrogen peroxide to bypass the interior of the catalyst can **221**. Similar passageways exist in the mixer **203**. These features are described in more detail below.

FIGS. 7 and 8 display the catalyst can **221**. The catalyst can **221** is preferably made from a suitable material, such as a high temperature, non-catalytic aerospace alloy. The catalyst can **221** has a cylindrical outer wall **241** with a flange **243**. The flange **243** includes a plurality of apertures **245**. Preferably, the flange **243** includes 12 equally spaced apertures **245**, each having a diameter of 0.050". Again, the size, number and arrangement of apertures could be adjusted to achieve a desired result. The apertures **245** are in communication with the gap **263** between the catalyst can **221** and the outer housing **207** to allow the bypass hydrogen peroxide to flow towards the mixer section **203**.

The interior of the catalyst can **221** has an annular groove **247** adjacent the upstream end. As seen in FIGS. 4 and 7, the groove **247** receives a metal ring **249**. The downstream end of the catalyst can **221** includes an annular shoulder **251**. As seen in FIG. 4, the contents within the catalyst can **221** are retained between the metal ring **249** and the shoulder **251**.

The contents of the catalyst can **221** include a second pressure baffle **253**, a third pressure baffle **255**, and catalyst material **257**. The second pressure baffle **253** is located adjacent the ring **249**. The second pressure baffle **253** is also preferably made from a high temperature, non-catalytic aerospace alloy. As seen in FIG. 9, the baffle **253** has an array of openings **259** therethrough. Preferably, the baffle **253** has an outer diameter of approximately 2.70" and the openings **259** have a diameter of approximately 0.093". However, other sizes, numbers and arrangements of the apertures **259** could be used to achieve a suitable result.

The ring **249** placed in the annular groove **247** retains the pressure baffle **253** in the catalyst can **221**. The baffle **253** serves to reduce the pressure of the liquid hydrogen peroxide in the direction of flow. In other words, the pressure of the hydrogen peroxide downstream of the baffle **253** is less than the pressure of the hydrogen peroxide upstream of the baffle.

The third pressure baffle **255** rests against the shoulder **251**. The third pressure baffle **255** is also preferably made from a high temperature, non-catalytic aerospace alloy. As seen in FIG. 10, the baffle **255** has an array of openings **261** therethrough. Preferably, the baffle **255** has an outer diameter of approximately 2.70" and the openings **261** have a

diameter of approximately 0.078". However, other sizes, numbers and arrangements of the apertures 261 could be used to achieve a suitable result.

The catalyst material 257 resides between the second pressure baffle 253 and the third pressure baffle 255. Preferably, the catalyst material 257 comprises a bed of silver alloy. However, any catalyst that is useful in decomposing the hydrogen peroxide could be used.

The assembly of the catalyst can 221 will now be described with reference to FIGS. 4, 5 and 7. First, the third pressure baffle 255 is seated on the shoulder 251 of the catalyst can 221. Next, the catalyst material 257 is placed into the catalyst can 221. Then, the second pressure baffle 253 is placed into the catalyst can. Finally, the ring 249 is seated into the groove 247 of the catalyst can. The catalyst can 221 is now fully assembled.

Before the catalyst can 221 is placed into the outer housing 207, the first pressure baffle 223 is placed in the upstream end of the open interior 219 of the outer housing 207 and secured with the ring 235. The catalyst can 221 is then placed into the open interior 219 of the outer housing 207. The flange 243 of the catalyst can rest on the shoulder 231 of the outer housing 207. To ensure suitable retention, the catalyst can 221 can be secured to the outer housing 207 using suitable fasteners (not shown). Finally, the coupling 217 is secured to the opening 213 in the front face 215 of the outer housing 207. The catalyst bed section 201 is now fully assembled.

The catalyst bed section 201 preferably receives a uniform supply of liquid hydrogen peroxide to produce a constant discharge. Specifically, the supply pipe has a diameter of approximately 3" and supplies approximately 4-8 pounds per second of liquid hydrogen peroxide at a temperature of approximately 100° F. The catalyst bed section 201 decomposes the liquid hydrogen peroxide to produce a discharge. The mixer 203 receives this discharge, comprising water vapor and oxygen at approximately 750 psi and 2192° R.

FIG. 11 shows a perspective view of the mixer 203. The mixer 203 includes an inner housing 281 located within an outer housing 283. Both the inner housing 281 and the outer housing 283 are made from a suitable material, such as a high temperature, non-catalytic aerospace alloy.

FIG. 12a displays a cross-sectional view of the inner housing 281. The inner housing 281 has a cylindrical body 285 with a flange 287 at one end. The flange 287 includes a plurality of apertures 289. The apertures 289 preferably align with the apertures 245 on the flange 243 of the catalyst can 221 to form a passageway for the bypass hydrogen peroxide. To align with the apertures 245, the flange 287 should have 12 equally spaced apertures 289, each having a diameter of 0.050". Again, the size, number and arrangement of the apertures 289 could be adjusted to achieve the desired cooling of the mixer 203 by the bypass hydrogen peroxide. This feature will be explained in more detail below.

As seen in FIG. 12a, a plurality of fins 325 extend from the outer diameter of the inner housing 281. The fins 325 about the inner diameter of the outer housing 283 to align the inner housing 281 relative to the outer housing 283. This creates a gap 303 between the remainder of the inner housing 281 and the outer housing 283. The gap 303 allows the bypass hydrogen peroxide to flow between the inner housing 281 and the outer housing 283 of the mixer 203 for cooling. Since the fins 325 are circumferentially spaced from each other along the outer diameter of the inner housing 281, the bypass hydrogen peroxide can pass between adjacent fins 325 to exit towards the nozzle 205.

FIG. 12b displays a cross-sectional view of the outer housing 283. The outer housing 283 has a cylindrical body 291 with a flange 293 at one end and a flange 295 at the opposite end. The flanges 293, 295 include openings 297 for the fasteners F used to secure the sections 201, 203, 205 together. The one end of the outer housing 283 has a recess 298 that receives the flange 287 of the inner housing 281. The other end of the outer housing 283 includes a groove 299 that receives a seal 301 positioned between the mixer 203 and the nozzle 205. As described earlier, the seal 301 could be a C-shaped annular metal seal, or any other suitable seal.

FIG. 13 shows the inner housing 281 positioned within the outer housing 283 (and with the sections 201, 203, 205 secured together). The figure also clearly shows a path 305 (shown in dashed line) taken by the liquid bypass hydrogen peroxide. Specifically, the path 305 of the bypass hydrogen peroxide begins in the gap 263 between the catalyst can 221 and the outer housing 207 of the catalyst bed section 201. The bypass hydrogen peroxide then travels through the apertures 245 in the flange 243 of the catalyst can 221 and into the apertures 289 in the flange 287 of the inner housing 281. The bypass hydrogen peroxide then enters the gap 303 between the inner housing 281 and the outer housing 283 and past the fins 325 on the inner housing 281 to exit the mixer 203.

Since the nozzle 205 is likewise exposed to the heat created by the decomposition of the hydrogen peroxide in the catalyst can 221, heat build-up in the nozzle 205 must also be controlled. Similar to the annular gap 263 in the catalyst bed section and the annular gap 303 in the mixer 203, a gap 307 exists between the nozzle 205 and the catalyst can 221 downstream of the catalyst can 221. The bypass hydrogen peroxide travels along this gap 307 and into the interior section of the nozzle 205 where it merges with the decomposed hydrogen peroxide. Preferably, the liquid bypass hydrogen peroxide provides film cooling along the inner diameter of the nozzle 205.

Preferably, approximately 95 percent of the hydrogen peroxide introduced through coupling 217 and into the catalyst bed 201 enters the catalyst can 221. This portion of the hydrogen peroxide undergoes decomposition by the catalyst material 257.

The remaining 5 percent of the hydrogen peroxide bypasses around the catalyst can 221 and does not contact the catalyst material 257. As discussed above, this remainder of the liquid hydrogen peroxide is used to cool the gas generator 200. Although a 5 percent bypass percentage is discussed, any suitable percentage could be used. The amount of bypass could be controlled by the size of the annular gaps 263, 265, the gap 307, or by the number and the size of the apertures 245, 289 or fins 325.

The main purpose of the mixer 203 is to augment the constant discharge from the catalyst bed section 201 with a selected amount of additional mass flow. This additional amount increases the exhaust stream exiting the nozzle 205. Since the gas generator 200 is preferably part of a turbopump assembly, the turbine converts the increased mass flow of the exhaust stream into additional torque to drive the impeller. The increased torque on the impeller increases the supply of either the oxidizer or the fuel to the rocket engine. The increased supply of fuel or oxidizer to the rocket engine increases thrust. In other words, the mixer section 203 can be used to throttle the rocket engine.

To achieve this result, FIGS. 4 and 11 show the mixer 203 with openings 309 through the inner housing 281 and the

outer housing **283**. Opposite each opening **309**, the inner housing **281** includes a recess **311**. Each opening **309** and corresponding recess **311** receives a spray bar assembly **313**.

The spray bar assemblies **313** inject liquid hydrogen peroxide into the discharge within the inner housing **281** of the mixer **203**. Due to the temperature of the discharge 5
2192° R), the injected liquid hydrogen peroxide will decompose merely upon exposure to the discharge. In other words, the injected liquid hydrogen peroxide decomposes even without exposure to the catalyst material **257** in the catalyst bed section **201**. 10

Although FIG. **11** displays that the mixer **203** could receive three spray bar assemblies **313**, any number is possible. In addition, although FIG. **15** displays the spray bar assemblies centrally located within the mixer, the position of the spray bar assemblies **313** could be adjusted to achieved a desired result. 15

The spray bar assembly **313** includes a body **315** secured to the mixer **203** and a coupling **317** threaded into the body **315**. The coupling **317** receives a pipe (shown in phantom in FIG. **14**) supplying hydrogen peroxide to the mixer **203**. The spray bar assembly **313** also includes a tube **319**. Preferably, the tube **319** is made from a suitable high temperature, non-catalytic aerospace alloy and has a diameter of approximately 0.500", although any suitable size could be used. 20

The tube **319** has one end **321** located within the body **315**. The tube **319** has ports **323** arrayed along the other end located within mixer **203**. Preferably, the ports **323** have a diameter of approximately 0.040". A pump (not shown) can be used to inject the liquid hydrogen peroxide into the mixer **203**. The liquid hydrogen peroxide travels from the pipe, into the body **315**, down the tube **319** and through the ports **323** into the mixer **203**. Although the spray bar assembly **313** has been described as using a pump, any other mechanism (e.g. a venturi tube) could be used to inject the hydrogen peroxide into the mixer **203**. 25

Preferably, the amount of liquid hydrogen peroxide supplied to the spray bar assemblies **313** is selected to achieve a desired mass flow of the exhaust stream exiting the nozzle **205**. For example, each spray bar assembly could inject approximately 4 pounds per second of hydrogen peroxide at 30

approximately 750 psi into the mixer **203**. The hydrogen peroxide supplied to the mixer **203** could be from the same source as the hydrogen peroxide supplied to the catalyst bed section **201**. Other arrangements, such as discrete sources, could be used.

FIG. **11** shows various other openings in the mixer **203** that receive conventional thermocouples (not shown) to sense the temperature within the gas generator **200**. These conventional features will not be discussed in further detail.

The present invention has been described in connection with the preferred embodiments of the various figures. It is to be understood that other similar embodiments may be used or modifications and additions may be made to the described embodiment for performing the same function of the present invention without deviating therefrom. Therefore, the present invention should not be limited to any single embodiment, but rather construed in breadth and scope in accordance with the recitation of the appended claims. 35

What is claimed is:

1. A gas generator, comprising:

a catalyst section, said catalyst section including openings through which a material enters and reacts with a catalyst to decompose and to produce heat; and

a mixer section downstream of said catalyst section, said mixer section introducing an additional amount of said material;

wherein said heat produced in said catalyst section is sufficient to decompose said additional amount of said material without exposure to said catalyst. 40

2. The gas generator as recited in claim **1**, wherein said material is hydrogen peroxide.

3. The gas generator as recited in claim **1**, further comprising a nozzle downstream of said mixer section.

4. The gas generator as recited in claim **1**, wherein said additional amount also cools said catalyst section.

5. The gas generator of claim **1**, wherein said gas generator is part of a turbopump assembly.

* * * * *